

# Measurement of the effective temperature of majority carriers under injection of hot minority carriers in heterostructures

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(Received 20 September 1993; accepted for publication 19 February 1994)

We propose and demonstrate a purely electrical method for measuring the effective temperature  $T_e$  of majority carriers under the injection of hot minority carriers. The  $T_e$  of holes in a thin  $p$ -type InGaAs layer, heated by electron injection from an InAlAs layer in a three-terminal lattice-matched heterostructure, was determined by measuring the thermionic emission current of holes over another specially designed InGaAs/InAlAs barrier. At  $T=77$  K, we observed an overheating  $T_e - T$  of over 50 K, even at moderate injection power levels.

Injection of hot minority carriers is a common phenomenon in modern heterojunction devices. Electrons injected at high energy, corresponding to the conduction band discontinuity, thermalize via optical phonon emission and inelastic scattering by majority holes. As a result, the effective temperature  $T_e$  of holes in the active region may significantly depart from the lattice temperature  $T$ . The increasing  $T_e$  leads to an enhancement of the thermionic flow of holes from the active region and increases the intensity of Auger recombination processes. Overheating of majority carriers may have important consequences for the performance of such heterostructure devices as lasers, bipolar transistors, etc.

It is possible to estimate  $T_e$  from the high-energy tails of interband luminescence spectra,<sup>1</sup> when such spectra can be taken from the active region. Recently, we employed the electroluminescence technique to measure the temperature of an electron-hole plasma in complementary real-space transfer transistors at high injection current densities.<sup>2</sup> We observed a strong overheating  $\Delta T_e = T_e - T \geq 100$  K. In the present letter, we propose and experimentally demonstrate an *electrical* method for the determination of  $T_e$ , based on monitoring the thermionic current of majority carriers. In contrast to electroluminescence experiments, this method (i) does not require a high radiative efficiency of interband recombination and (ii) allows us to estimate  $\Delta T_e$  at low injection levels.

The three-terminal heterostructure device used in our experiments is illustrated in Fig. 1. The lattice-matched InGaAs/InAlAs heterostructure was grown by molecular beam epitaxy on a conducting InP substrate and processed into devices using optical lithography and selective wet etching. A key fabrication step involved evaporation of self-aligned ohmic contacts to the  $p$ -type active layer, as described in Ref. 2. The distance between these contacts was  $L=2$   $\mu\text{m}$ . We used devices with the widths  $W=10$  and  $20$   $\mu\text{m}$ , defining the collector area  $W \times L$ . The total injector area, defined by a mesa etch, was  $0.96$  and  $1.35 \times 10^{-5}$   $\text{cm}^2$  for  $10$  and  $20$   $\mu\text{m}$  devices, respectively.

The bottom of Fig. 1 shows the device band diagram (in the plane that cuts the collector in the middle) under bias. Both ohmic contacts to the active layer are grounded and negative voltages are applied both to the injector ( $-V_E$ ) and the collector ( $-V_C$ ). In the operating regime, electrons are injected into the active layer with an initial kinetic energy

equal to the conduction band discontinuity  $\Delta E_C=0.5$  eV and holes flow into the collector thermionically over the valence band barrier  $\Delta E_V=0.2$  eV (these are generally accepted<sup>3,4</sup> values for the  $\text{In}_{0.53}\text{Ga}_{0.47}\text{As}/\text{In}_{0.52}\text{Al}_{0.48}\text{As}$  heterosystem). The value of  $\Delta E_V$  in the present sample was confirmed by studying the temperature dependence of the thermionic current of holes from the active region into the collector at zero injection bias  $V_E=0$  and low collector bias  $V_C=0.1$  V. Assuming  $\Delta E_V=0.2$  eV, the obtained dependence of the collector current  $I_C(T)$  in the range  $150 \leq T \leq 250$  K is in a good agreement with the thermionic model,  $I_C = SA^* T^2 \exp(-\Phi/kT)$ , where  $S$  is the barrier area (we studied two type of samples with  $S=2$  and  $4 \times 10^{-7}$   $\text{cm}^2$ ),  $A^* \approx 60$   $\text{A}/\text{cm}^2 \text{K}^2$  is the effective Richardson constant,  $\Phi = \Delta E_V + E_{Fp}$  is the thermionic barrier for holes, and  $E_{Fp}$  is the hole Fermi level in the active region.

Figure 2 shows a typical dependence  $I_C(V_C)$  measured at  $T=77$  K and different injection current densities  $J_E$ . Polarity of the current corresponds to holes flowing into the collector. The collector current nearly saturates at high  $V_C$  with a residual increase that can be attributed to a barrier lowering. When the negative potential of the active region

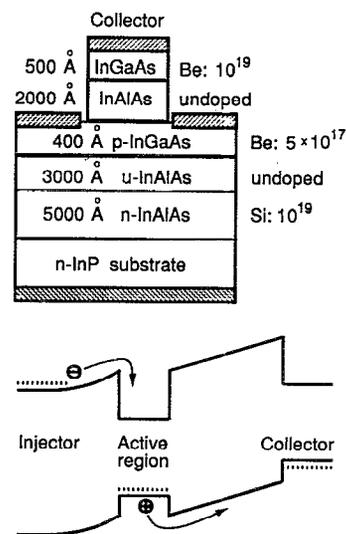


FIG. 1. Structure cross section and the band diagram under bias.

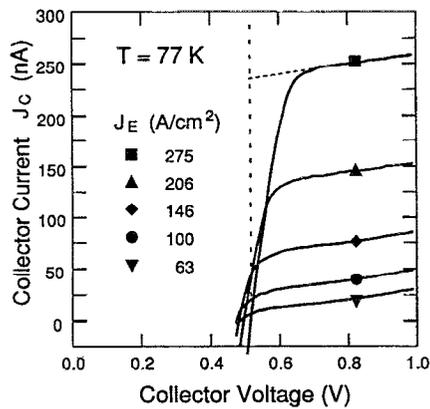


FIG. 2. Dependence of the collector current  $I_C$  on the collector voltage  $V_C$  for several injection current densities  $J_E$ . The collector area is  $2 \mu\text{m} \times 10 \mu\text{m} = 2 \times 10^{-7} \text{cm}^2$ . Dashed line illustrates the procedure of extrapolating to the flatband condition.

under the collector is lower than  $V_C$ , then the collector current flows in the opposite direction, since the valence band discontinuity does not present a barrier for the flow of holes from the heavily doped collector with no setback layer. The point where  $I_C$  changes sign corresponds approximately to the flatband condition. We are using this consideration to extrapolate the thermionic current  $I_C$ , measured at higher  $V_C$ , to the flatband value. In Fig. 2, the extrapolation is illustrated by the dashed lines for the case  $J_E = 275 \text{A/cm}^2$ .

The extrapolated value of the collector current density  $J_C$  is plotted in Fig. 3 against the injection current density  $J_E$ . The effective temperature of holes was then estimated by the thermionic formula

$$J_C = A^* T_e^2 e^{-\Phi/kT_e},$$

using the above values of  $A^*$  and  $\Delta E_V$ . The variation of the barrier height  $\Phi = \Delta E_V + E_{FP}$  due to the dependence of  $E_{FP}$

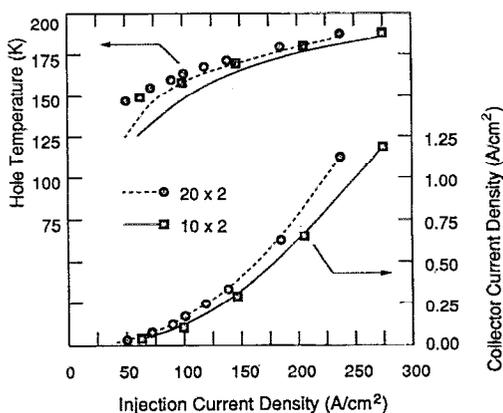


FIG. 3. Dependence of the collector current density  $J_C$  at flatbands and the effective hole temperature  $T_e$  on the injection current density  $J_E$ . In the  $T_e$  plot, the symbols designate the temperature calculated that the thermionic emission of holes is the only mechanism of collector current, whereas the lines indicate an adjusted behavior of  $T_e$ , assuming a probability of  $\xi = 6 \times 10^{-4}$  for direct impact emission channels.

on the carrier temperature was included self-consistently. The slight adjustment of  $E_{FP}$  due to the injected carrier density was also included, assuming a carrier lifetime  $\tau = 10^{-9} \text{s}$  in the active region. Since the estimated injected electron density is less than the majority carrier density  $p = 5 \times 10^{17} \text{cm}^{-3}$ , provided by Be doping, the Fermi level  $E_{FP}$  of holes varies little with injection and the possible error in the assumed value of  $\tau$  has no significant effect on our estimate of  $T_e$ .

Thus, calculated  $T_e$  is indicated in Fig. 3 by shaded squares and circles for two measured samples. We see that the amount of overheating  $\Delta T_e \approx 75 \text{K}$  is quite substantial even for moderate injection current levels. The curve  $T_e(J_E)$  does not seem to extrapolate to  $77 \text{K}$  at low  $J_E$ ; a possible explanation for this will be discussed below. Thermal conductivity estimates<sup>5</sup> show that the expected overheating of the lattice itself is negligible (less than  $1 \text{K}$ ) in our experiments. This agrees with our earlier observation<sup>2</sup> of no significant lattice heating, deduced from electroluminescence measurements at much higher injection densities. Additional evidence that joule heating effects are negligible comes from the tendency of  $T_e$  to saturate with increasing  $J_E$ , as well as from the fact that we have seen no superexponential behavior in the injector diode characteristic.

Assuming that the incoming power density equals  $(J_E/ed)\Delta E_C$ , where  $d = 400 \text{\AA}$  is the active layer thickness, we estimate that the energy relaxation time  $\tau_e$  of holes in our experiment is more than  $10 \text{ps}$ . This appears to be somewhat longer but reasonably close to what one can expect in InGaAs. However, much longer values of  $\tau_e$  would be estimated at lower  $J_E$ , where we do not observe the expected tendency  $T_e \rightarrow T$ .

A possible explanation for this discrepancy may be associated with our neglect of direct impact emission of holes by high energy electrons, prior to thermalization. Under the conditions of our experiment, the electron-hole interaction is dominated<sup>6</sup> by scattering channels in which heavy holes are transformed into light holes with high kinetic energy. Presumably, similar considerations apply to channels in which holes end up in the split-off band. Although the probability of a direct emission of such holes should be low, the resultant collector current density scales linear with  $J_E$  and should be dominant at low injection, since the thermionic component decreases exponentially. Taking into account this contribution would not alter our estimates for  $T_e$  at high injection levels, but those at low injection levels would be drastically changed. Assuming a probability  $\xi$  of the direct impact emission we can subtract the contribution  $J_C = \xi J_E$  and recalculate the carrier temperature; this procedure is illustrated in Fig. 3, where we assumed  $\xi \approx 6 \times 10^{-4}$ . Obviously, thus defined curves  $T_e(J_E)$  automatically extrapolate to the lattice temperature as  $J_E \rightarrow 0$ .

The difference between the calculated temperatures displayed in Fig. 3 and the ambient temperatures, corresponding to the same value of  $J_C$  obtained in thermionic experiments, increases with  $J_E$  but even at the highest injection levels it is less than 5% of the estimated value of  $T_e$ . A possible origin of this discrepancy may be attributed to a dependence of the

carrier lifetime on the concentration and the effective temperature.

In conclusion, we proposed and demonstrated an electrical method for measuring the effective carrier temperature in heterostructures. One of the advantages of this method is that it makes possible estimates of majority carrier overheating in structures with a low radiative efficiency of interband transitions. This offers an opportunity for studying the overheating effects in the base of a heterojunction bipolar transistor. Sensitivity of the method allows measurements at low injected power densities.

We wish to thank N. K. Dutta, M. Frei, R. Hamm, R. F.

Kazarinov, and M. Mastrapasqua for useful discussions and assistance and T. R. Fullowan for silicon nitride deposition.

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<sup>5</sup>M. Frei (private communication).

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